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Viscous Dissipation and Heat Absorption effect on Natural Convection Flow with Uniform Surface Temperature along a Vertical Wavy Surface

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ABSTRACT

The effect of viscous dissipation and heat absorption on a steady two-dimensional natural convection laminar flow of viscous incompressible fluid with uniform surface temperature along a vertical wavy surface has been investigated. Using the appropriate variables; the basic equations are transformed to convenient form and then solved numerically employing very efficient method, namely Keller-Box method (KBM). Numerical results are presented by the shearing stress in terms of the local skin-friction coefficient; the rate of heat transfer in terms of local Nusselt number, streamline and isotherms, respectively for a wide range of the viscous dissipation parameter N and heat absorption parameter Q . Increasing Q and lessening N cause the enhancement of heat transfer rate.

KEYWORDS: Viscous dissipation; Heat absorption; Natural convection; Keller-Box method; Wavy surface.

MSC (2010) No.: 76D05, 76R10

1. INTRODUCTION

Many scientists investigated viscous dissipation for various purposes in science separately or in presence of heat generation or heat absorption. Gebhart (1962) studied the effects of viscous dissipation in natural convection and then in external natural convection flow

together with Mollendorf (1969). Natural convection was introduced along a vertical wavy surface by Yao (1983). Vajravelu and Hadjinolaou (1993) studied the heat transfer characteristics in the laminar boundary layer of a viscous fluid over a stretching sheet with viscous dissipation or frictional heating and internal heat generation. In this study they considered that the volumetric rate of heat generation, $q''' [W/m^3]$, should be $q''' = Q_0(T - T_\infty)$, for $T \geq T_\infty$ and equal to zero for $T < T_\infty$, where Q_0 is the heat generation/absorption constant. Hossain and Rees (1999) first investigated combined heat and mass transfer in natural convection flow from a vertical wavy surface and then Jang et al. (2003) investigated natural convection heat and mass transfer along a vertical wavy surface. Molla et al. (2004) studied natural convection flow along a vertical wavy surface with uniform surface temperature in presence of heat generation/absorption.

Alam et al. (2007) investigated viscous dissipation effects on MHD natural convection flow over a sphere in the presence of heat generation. Mamun et al. (2008) analyzed MHD-conjugate heat transfer analysis for a vertical flat plate in presence of viscous dissipation and heat generation. Devi and Kayalvizhi (2010) considered viscous dissipation and radiation effects on the thermal boundary layer flow with heat and mass transfer over a non-isothermal stretching sheet with internal heat generation embedded in a porous medium. Jha and Ajibade (2011) studied effect of viscous dissipation on natural convection flow between vertical parallel plates with time-periodic boundary conditions. Joule heating and viscous dissipation effects were investigated on MHD flow past a semi-infinite inclined plate with variable surface temperature by Palani and Kim (2011). Recently, Parveen and Alim (2012) have observed the effects of MHD natural convection flow along a vertical wavy surface in presence of heat generation/absorption with viscosity dependent on temperature.

From the above one thing is clear that yet it has not been justified the effects of viscous dissipation and heat absorption together on natural convection flow along a vertical wavy surface. The object of the study is to show the effect of our present work.

2. FORMULATION OF THE PROBLEM

The boundary layer analysis outlined below allows $\bar{\sigma}(X)$ being arbitrary, but our detailed numerical work assumed that the surface exhibits sinusoidal deformations. The wavy surface may be described by

$$Y_w = \bar{\sigma}(X) = \alpha \sin\left(\frac{n\pi X}{L}\right), \quad (1)$$

where L is the wave length associated with the wavy surface.

The geometry of the wavy surface and the two-dimensional Cartesian coordinate system are shown in Figure 1.

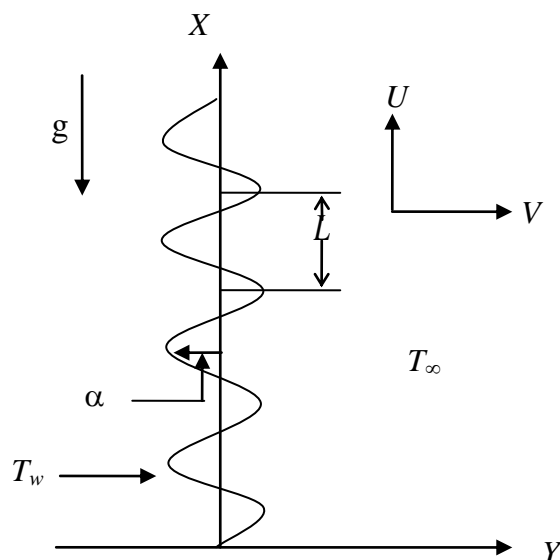


Figure 1. The coordinate system and the physical model

The conservation equations for the flow characterized with steady, laminar and two-dimensional boundary layer; under the usual Boussinesq approximation, dimensionless form of the continuity, momentum and energy equations can be written as:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0, \quad (2)$$

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = -\frac{\partial p}{\partial x} + Gr^{1/4} \sigma_x \frac{\partial p}{\partial y} + (1 + \sigma_x^2) \frac{\partial^2 u}{\partial y^2} + \theta, \quad (3)$$

$$\sigma_x \left(u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} \right) = -Gr^{1/4} \frac{\partial p}{\partial y} + \sigma_x (1 + \sigma_x^2) \frac{\partial^2 u}{\partial y^2} - \sigma_{xx} u^2, \quad (4)$$

$$u \frac{\partial \theta}{\partial x} + v \frac{\partial \theta}{\partial y} = \frac{1}{Pr} (1 + \sigma_x^2) \frac{\partial^2 \theta}{\partial y^2} + Q\theta + N \left(\frac{\partial u}{\partial y} \right)^2, \quad (5)$$

where $Pr = \frac{C_p \mu}{k}$ is the Prandtl number, $Q = \frac{Q_0 L^2}{\mu C_p Gr^{1/2}}$ is the heat absorption parameter

and $N = \frac{\nu^2 Gr}{L^2 C_p (T_w - T_\infty)}$ is the viscous dissipation parameter.

The following dimensionless variables are introduced for non-dimensionalizing the governing equations,

$$x = \frac{X}{L}, \quad y = \frac{Y - \bar{\sigma}}{L} Gr^{1/4}, \quad p = \frac{L^2}{\rho \nu^2} Gr^{-1} P, \quad u = \frac{L}{\nu} Gr^{-1/2} U, \quad v = \frac{L}{\nu} Gr^{-1/4} (V - \sigma_x U)$$

$$\theta = \frac{T - T_\infty}{T_w - T_\infty}, \quad \sigma_x = \frac{d\bar{\sigma}}{dX} = \frac{d\sigma}{dx}, \quad Gr = \frac{g\beta(T_w - T_\infty)}{\nu^2} L^3,$$

where θ is the non-dimensional temperature function and (u, v) are the dimensionless velocity components.

It can easily be seen that the convection induced by the wavy surface is described by equations (2)–(5). We further notice that, equation (5) indicates that the pressure gradient along the y -direction is $O(Gr^{-1/4})$, which implies that lowest order pressure gradient along x -direction can be determined from the inviscid flow solution. For the present problem this pressure gradient ($\partial p/\partial x = 0$) is zero. Equation (4) further shows that $Gr^{1/4}\partial p/\partial y$ is $O(1)$ and is determined by the left-hand side of this equation. Thus, the elimination of $\partial p/\partial y$ from equations (3) and (4) leads to

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = \left(1 + \sigma_x^2\right) \frac{\partial^2 u}{\partial y^2} - \frac{\sigma_x \sigma_{xx}}{1 + \sigma_x^2} u^2 + \frac{1}{1 + \sigma_x^2} \theta. \quad (6)$$

The corresponding boundary conditions for the present problem are:

$$\left. \begin{aligned} u = v = 0, \quad \theta = 1, \quad \text{at } y = 0, \\ u = \theta = 0, \quad p = 0, \quad \text{as } y \rightarrow \infty. \end{aligned} \right\} \quad (7)$$

Now we introduce the following transformations to reduce the governing equations to a convenient form:

$$\psi = x^{3/4} f(x, \eta), \quad \eta = yx^{-1/4}, \quad \theta = \theta(x, \eta). \quad (8)$$

Introducing the transformations given in Equation (8) and into Equation (6) and (5), the following system of nonlinear equations are obtained

$$\left(1 + \sigma_x^2\right) f''' + \frac{3}{4} f f'' - \left(\frac{1}{2} + \frac{x \sigma_x \sigma_{xx}}{1 + \sigma_x^2}\right) f'^2 + \frac{1}{1 + \sigma_x^2} \theta = x \left(f' \frac{\partial f'}{\partial x} - f'' \frac{\partial f}{\partial x} \right), \quad (9)$$

$$\frac{1}{\text{Pr}} \left(1 + \sigma_x^2\right) \theta'' + \frac{3}{4} f \theta' + x^{1/2} Q \theta + N x f''^2 = x \left(f' \frac{\partial \theta}{\partial x} - \theta' \frac{\partial f}{\partial x} \right). \quad (10)$$

The boundary conditions (7) now take the following form:

$$\left. \begin{aligned} f(x, 0) = f'(x, 0) = 0, \quad \theta(x, 0) = 1, \\ f'(x, \infty) = 0, \quad \theta(x, \infty) = 0. \end{aligned} \right\} \quad (11)$$

The local skin friction coefficient C_{fx} and the rate of heat transfer in terms of the local Nusselt number Nu_x takes the following form:

$$C_{fx} (Gr/x)^{1/4} / 2 = \sqrt{1 + \sigma_x^2} f''(x, 0), \quad (12)$$

$$Nu_x (Gr/x)^{-1/4} = -\sqrt{1 + \sigma_x^2} \theta'(x, 0). \quad (13)$$

3. METHOD OF SOLUTION

The governing equations are solved numerically with the help of implicit finite difference method together with the Keller-Box scheme (1974). The discretization of momentum and energy equations are carried out with respect to non-dimensional coordinates x and η to convey the equations in finite difference form by approximating the functions and their derivatives in terms of central differences in both the coordinate directions. Then the required equations are to be linearized by using the Newton's Quasi-linearization method. The linear algebraic equations can be written in a block matrix which forms a coefficient matrix. The whole procedure namely reduction to first order followed by central difference approximations, Newton's Quasi-linearization method and the block Thomas algorithm, is well known as Keller-box method.

4. RESULTS AND DISCUSSION

Here we have shown the combined effects of viscous dissipation and heat absorption on natural convection flow of viscous incompressible fluid along a vertical wavy surface. The skin friction coefficient C_{fx} , the rate of heat transfer in terms of Nusselt number Nu_x , the streamlines as well as the isotherms are shown graphically in Figures 2 to 5 for different values of the heat absorption parameter Q and the viscous dissipation parameter N .

From the Figures 2(a) and (b), it is noted that the higher value of N accelerates the fluid flow and increases the temperature so with the increasing of viscous dissipation parameter $N = (0.0, 0.4, 1.0, 1.5, 2.0)$, the skin friction coefficient C_{fx} increases along the upstream direction of the surface and the heat transfer rates in terms of the local Nusselt number Nu_x decreases.

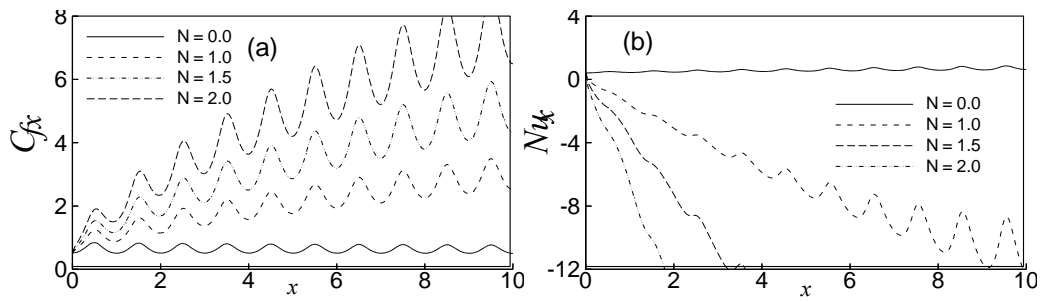


Figure 2. Effect of N on (a) skin friction coefficient C_{fx} and (b) rate of heat transfer Nu_x while $\alpha = 0.3$ and $Pr = 1.73$

From Figures 3(a) and (b), it is observed that the heat absorption mechanism does not create a layer of hot fluid near the surface so the temperature of the fluid decreases the surface temperature and temperature gradient increases. Thus the values of heat absorption parameter $Q = (0.0, -0.2, -0.5, -0.8)$ leads to decrease the local skin friction coefficient C_{fx} and increase the local rate of heat transfer Nu_x at different position of x .

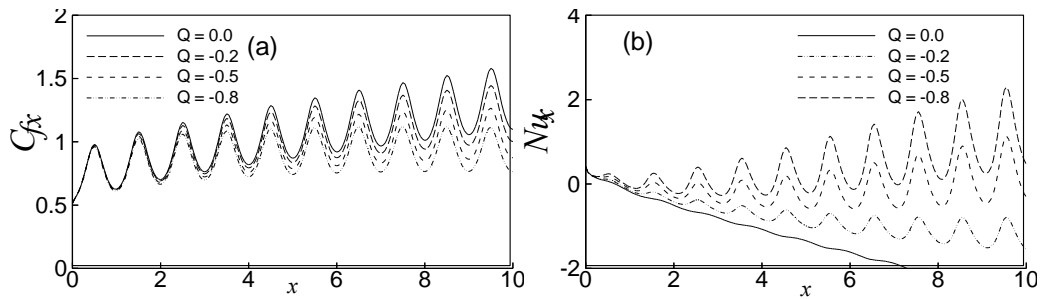


Figure 3. Effect of Q on (a) skin friction coefficient C_{fx} and (b) rate of heat transfer Nu_x while $\alpha = 0.3$ and $Pr = 1.73$

Figures 4 and 5 show the with and without effect of viscous dissipation parameter N and heat absorption parameter Q together on the formulation of streamlines and isotherms respectively while $Pr = 1.73$ and $\alpha = 0.3$. It is noted that with the effect of N , the velocity boundary layer becomes thicker and when Q increases the opposite results observed. The thermal boundary layer becomes thicker gradually for the effect of N . The temperature distribution decreases in presence of heat absorption parameter Q . The maximum value of ψ_{max} is 23.86 for $N = 2.0$.

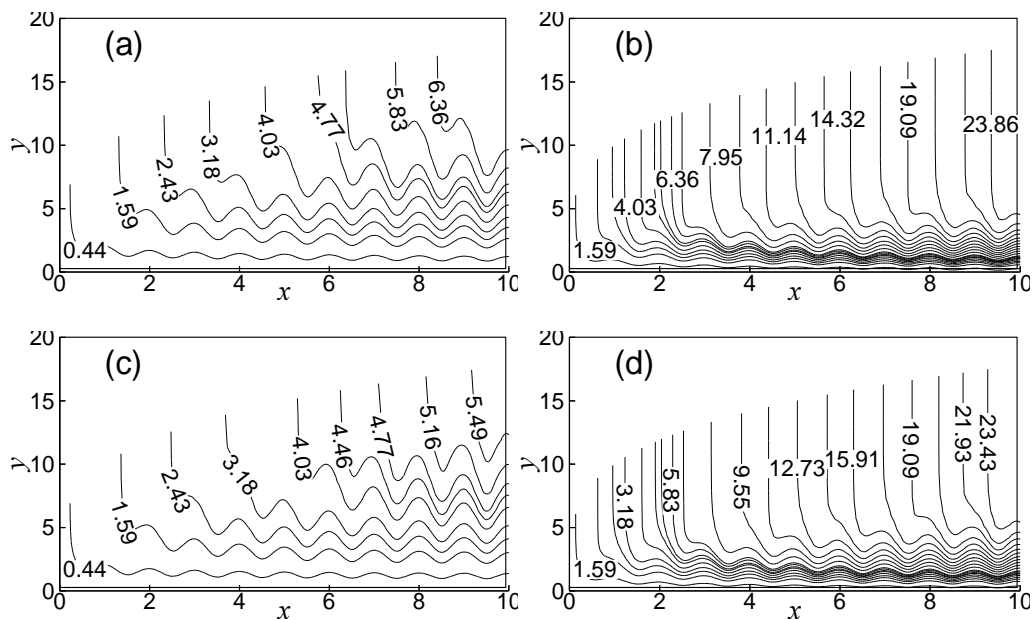


Figure 4. Streamlines for (a) $N = 0.0, Q = 0.0$ (b) $N = 2.0, Q = 0.0$ (c) $N = 0.0, Q = -0.8$ and (d) $N = 2.0, Q = -0.8$ while $Pr = 1.73$ and $\alpha = 0.3$

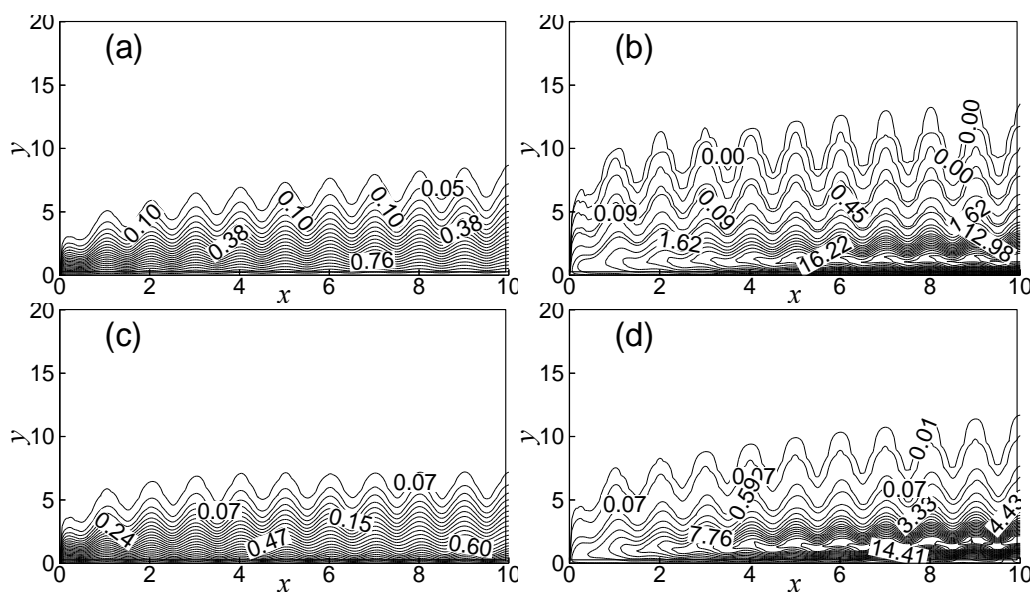


Figure 5. Isotherms for (a) $N = 0.0, Q = 0.0$ (b) $N = 2.0, Q = 0.0$ (c) $N = 0.0, Q = -0.8$ and (d) $N = 2.0, Q = -0.8$ while $Pr = 1.73$ and $\alpha = 0.3$

5. CONCLUSION

The effects of the heat absorption parameter Q and the viscous dissipation parameter N on natural convection flow of viscous incompressible fluid along a vertical wavy surface have been investigated. From the present investigation the following conclusions may be drawn:

- The skin friction coefficient C_{fx} has increased and the rate of heat transfer in terms of Nusselt number Nu_x has decreased for increasing values of N and opposite results has happened for heat absorption parameter Q .
- Streamlines have changed slightly too upper and the same results are observed for thermal boundary layer thickness with the increasing values of viscous dissipation parameter N and opposite results have observed for heat absorption parameter Q .

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